



# The SPH density estimate





From density to hydrodynamics

$$L_{sph} = \sum_{j} m_{j} \left[ \frac{1}{2} v_{j}^{2} - u_{j}(\rho_{j}, s_{j}) \right] \qquad \text{Lagrangian}$$

$$du \stackrel{+}{=} \frac{P}{\rho^{2}} d\rho \qquad \text{1st law of thermodynamics}$$

$$\nabla \rho_{i} = \sum_{j} m_{j} \nabla W_{ij}(h) \qquad \text{density sum}$$

$$\frac{d}{dt} \left( \frac{\partial L}{\partial \mathbf{v}} \right) - \frac{\partial L}{\partial \mathbf{r}} = 0 \qquad \text{Euler-Lagrange equations}$$

$$= \qquad \text{equations}$$

$$d\mathbf{v}_{i} = -\sum_{j} m_{j} \left( \frac{P_{i}}{\rho_{i}^{2}} + \frac{P_{j}}{\rho_{j}^{2}} \right) \nabla_{i} W_{ij}(h) \qquad \left( \frac{d\mathbf{v}}{dt} = -\frac{\nabla P}{\rho} \right)$$

# What this gives us: Advantages of SPH

- An exact solution to the continuity equation
- Resolution follows mass, natural compatibility with N-body codes
- ZERO dissipation
- Advection done perfectly
- EXACT conservation of mass, momentum, angular momentum, energy and entropy
- A guaranteed minimum energy state









# But must treat discontinuities properly...



Viscosity only

# This issue has NOTHING to do with the Kelvin-Helmholtz instability

Price (2008, J. Comp. Phys.)







Figure 13. Density slices of, from top to bottom, GRID1, GRID3 and SPH3. The panels show the KH simulation at  $t = \tau_{KH}/3$ ,  $2\tau_{KH}/3$  and  $\tau_{KH}$ . simulations show clear growth of the KHI while this is completely absent in SPH.



Figure 14. A close up view of the SPH particles at the boundaries between the shearing layers (left) and closer zoom in (right) for SPH3 at  $\tau_{KH}$ . We can see empty layers formed through erroneous pressure forces due to improper density calculations at density gradients. Even though the two fluids are relative to each other, the gap is so large that proper fluid interaction is severely decreased or even absent.

Simulating fluids using SPH and grid techniques 977



nsity slices through the centre of the cloud at *t* = 0.25, 1.0, 1.75 and 2.5 T<sub>KH</sub>. From top (EXZO\_256), FLASH (FLASH\_256) and ART-HYDRO (ART-256). The grid simulations clearly s H, unlike the SPH simulations in which most of the gas remains in a single cold dense blow.



# But must treat discontinuities properly...





Viscosity + conductivity

# This issue has NOTHING to do with the Kelvin-Helmholtz instability

Price (2008, J. Comp. Phys.)

# Richtmyer-Meshkov Instability







#### The key is a good switch



**Figure 2.** As Fig. 1, but for SPH with standard ( $\alpha = 1$ ) or Morris & Monaghan (1997) artificial viscosity, as well as our new method (only every fifth particle is plotted). Also shown are the undamped wave (*solid*) and lower-amplitude sinusoidals (*dashed*). Only with our method the wave propagates undamped, very much like SPH without any viscosity, as in Fig. 1.

#### 6 Lee Cullen & Walter Dehnen



**Figure 6.** Steepening of a 1D sound wave: velocity and viscosity parameter vs. position for standard SPH, the M&M method, our new scheme, and Godunov particle hydrodynamics of first and second order (GPH, Cha & Whitworth 2003), each using 100 particles per wavelength. The solid curve in the top panel is the solution obtained with a high-resolution grid code.

#### Cullen & Dehnen (2010), see also Read & Heyfield (2011)

Use of these switches removes the main disadvantage of SPH as used in numerical cosmology

# Exact conservation

# Exact conservation: Advantages



Orbits are orbits... even when they're not aligned with any symmetry axis.

# Exact conservation: Disadvantages

• Calculations keep going, even when they're screwed up...



Orszag-Tang Vortex in MHD (c.f. Price & Monaghan 2005, Rosswog & Price 2007, Price 2010)



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Why "rpSPH" (Morris 1996, Abel 2010) is a bad idea



$$\frac{\mathrm{d}\mathbf{v}_i}{\mathrm{d}t} = \sum_j m_j \left(\frac{P_i - P_j}{\rho_j^2}\right) \nabla_i W_{ij}$$

Improving the gradient operator leads to WORSE results

Corollary: Better to use a worse but conservative gradient operator

# Corollary: Need positive pressures





# 2D shock tube



# Why you cannot use "more neighbours" (or: How to halve your resolution)



N<sub>neigh</sub> should NOT be a free parameter!

i.e., should not change the ratio of smoothing length to particle spacing

# 2D shock tube



# Grid vs. SPH: Turbulence

Price & Federrath (2010): Comparison of driven, supersonic, isothermal turbulence





# Slice:



## Kinetic energy spectra (time averaged)



# But SPH resolution is in density field









![](_page_22_Figure_0.jpeg)

Figure 3. Visual comparison of the turbulent velocity field (top row), the density field (middle row) and the enstrophy  $|\nabla \times v|^2$  (bottom row) in quasi-stationary turbulence with  $\mathcal{M} \sim 0.3$ , simulated with different numerical techniques. Shown are thin slices through the middle of the perdiodic simulation box. From left to right, we show our moving grid result, an equivalent calculation on a static mesh, and an SPH calculation, as labeled.

![](_page_22_Figure_2.jpeg)

#### BS explanation:

We argue that the origin of this noise lies in errors of SPH's gradient estimate. Numerous studies have pointed out that the standard approach followed in SPH for constructing derivatives of smoothed fluid quantities involves rather large error terms, especially for the comparatively irregular particle distributions in multidimensional simulations. The problem lies in a lack of consistency of the ordinary density estimates (which do not conserve volume, i.e. the sum of  $m_i/\rho_i$  is not guaranteed to add up to the total volume) and in a low order of the gradient estimate itself (e.g. Quinlan et al. 2006; Gaburov & Nitadori 2011; Amicarelli et al. 2011). In practice, this means that there can be pressure forces on particles even though all individual pressure values of the particles are equal,

#### A clue:

port. To suppress the artificial viscosity in regions of strong shear, Balsara (1995) proposed a simple viscosity limiter in the form of an additional multiplicative factor  $(f_i + f_j)/2$  for the viscous tensor, defined as

$$f_i = \frac{|\nabla \cdot \boldsymbol{v}|_i}{|\nabla \cdot \boldsymbol{v}|_i + |\nabla \times \boldsymbol{v}|_i}.$$
(3)

This limiter is often used in cosmological SPH simulations and also available in the GADGET code. In our default simulations, we have refrained from enabling it, but we have also run comparison simulations where it is used, as discussed in our results section.

![](_page_24_Figure_0.jpeg)

# But what is the Reynolds number?

$$\mathcal{R}_{\rm e} \equiv \frac{VL}{\nu}$$

Stokes (1851), Reynolds (1883)

## **Dissipation in SPH**

There is none (it is a Hamiltonian system) ...except what you explicitly add.

AV terms give:

$$\nu \approx \frac{1}{10} \alpha v_{\rm sig} h; \qquad \zeta \approx \frac{1}{6} \alpha v_{\rm sig} h$$

Monaghan & Lattanzio (1985):  $\alpha = 1$ 

Morris & Monaghan (1997):  $\alpha$  (x, t)  $\in$  [0.1,1]

# Reynolds numbers in SPH $\mathcal{R}_{e} = \frac{10}{\alpha} \mathcal{M} \frac{L}{h},$ Price & Federrath (2010), Mach 10: $\int_{a}^{a} \int_{a}^{a} \int_{a}^{$

# Reynolds numbers in SPH

$$\mathcal{R}_{\rm e} = \frac{10}{\alpha} \mathcal{M} \frac{L}{h}, \qquad \begin{array}{l} \text{Linear} \\ \text{dependence on} \\ \text{Mach number} \end{array}$$

$$\mathcal{R}_{\rm e} = 2.4 n^{1/3} \left(\frac{\mathcal{M}}{0.3}\right) \left(\frac{\alpha}{1.0}\right)^{-1} \left(\frac{N_{\rm ngb}}{64}\right)^{-1/3}, \qquad \begin{array}{l} \end{array}$$

## In BS calculations:

$n = 64^3$	$n = 128^3$	$n = 256^3$
$\mathcal{R}_{\rm e} = 154$	$\mathcal{R}_{\rm e} = 307$	$\mathcal{R}_{\rm e} = 614$

# Using standard (15yo) viscosity switches:

![](_page_26_Figure_5.jpeg)

see also Dolag et al. (2005) and Valdarnini (2011) on importance of viscosity switches for SPH simulations of ICM/IGM turbulence

Also, much better viscosity switches now available (e.g. Cullen & Dehnen 2010)

![](_page_27_Figure_0.jpeg)

$$\begin{split} \mathcal{R}_{e} = \frac{v L}{v}, \end{split} (1) \\ \text{where } V \text{ is the flow velocity, } L \text{ is a typical length-scale, } v \text{ is the sound speed. Physically, these parameters estimate the relative importance of each of the terms in the Navier–Stokes equations – the Mach number specifies the ratio of the interial term, (v : <math>\nabla P_{e}$$
, to the pressure term,  $\nabla P_{e}$ , while the Reynolds number specifies the ratio of the interial term (v :  $\nabla P_{e}$ , to the pressure term,  $\nabla P_{e}$ , while the Reynolds number specifies the ratio of the interial term (v :  $\nabla P_{e}$ , to the pressure term,  $\nabla P_{e}$ , while the Reynolds number specifies the ratio of the interial term (v in the viscous dissipation term,  $\nabla V^{2}$ , Mathematically, these two parameters – along with the boundary conditions and driving – entirely characterize the flow. Given the importance of turbulence in theoretical models, it is crucial that agreement can be found between codes used for simulations of the ISM and ICM/IGM. Several comparison projects have been published recently comparing simulations of both decaying

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(Kitsionas et al. 2009) and driven (Price & Federrath 2010a) supersonic turbulence relevant to molecular clouds. However, fewer calculations appropriate to the ICM or IGM have been performed. In a recent preprint, Bauer & Springel (2011) have set out to extend the high Mach number comparisons to the mildly compressible, driven, subsonic turbulence throught to be appropriate to the ICM and IGM. In this case, the motions are comparable to or smaller than the sound speed, turbelet motions are dissipated by viscosity, and the flow is mainly characterized by the Reynolds number, similar to turbulence in the laboratory. In particular, it is well known from laboratory studies that the transition from laminar flow to fully developed turbulence only occurs once a critical Reynolds number is sobserved for  $\mathcal{R}_{\chi} \geq 2000$  (e.g. Reynolds 1895). Since at 100 Mach number the Reynolds number of solutiveluce, but also the character of such urbulence (e.g. the extent of the inertial range), it is critical to specify, or at least estimate, the Reynolds number set induced (2004) estimate  $\mathcal{R}_{\chi} \sim 10^3$ -10<sup>6</sup> for the cold ISM [so the approach adopted has been to fix the Mach number and try to reach high numerical Reynolds numbers are high specific and the Mach number and try to reach scale (2004) estimate  $\mathcal{R}_{\chi} \sim 10^3$ -10<sup>7</sup> or the cold ISM [so the approach adopted has been to fix the Mach number and try to reach high numerical Reynolds.

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1 256  $-128^{3}$ 64<sup>3</sup> 10-1 k<sup>5/3</sup> P(k) 10-2 10-3 10  $10^{2}$ k

Figure 2. Time-averaged  $k^{5/3}$ -compensated power spectra from subsonic SPH turbulence calculations using the Morris & Monaghan (1997) viscosity switch at a resolution of 64<sup>3</sup>, 128<sup>3</sup> and 256<sup>3</sup> particles, as indicated, for which the corresponding Reynolds numbers are  $\sim 1500, 3000$  and 6000, respectively. The shaded regions show the  $1\sigma$  errors from the timeaveraging. At the highest Reynolds numbers a Kolmogorov-like  $k^{-5/3}$ slope is evident at large scales.

![](_page_27_Figure_11.jpeg)

![](_page_27_Picture_12.jpeg)

AREPC

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Figure 3. Visual comparison of the turbul turbulence with  $\mathcal{M} \sim 0.3$ , simulated wit to right, we show our moving grid result,

#### Are moving mesh schemes better, or just different?

![](_page_28_Figure_1.jpeg)

Hopkins (2012) arXiv:1206.5006

"...deviations from Kolmogorov occur around the resolution limit, but are of a different character."

**Figure 9.** Velocity power spectrum in sub-sonic ( $\mathcal{M} = 0.3$ ) driven, isothermal turbulence. Each simulation uses  $128^3$  particles and identical driving. We compare the analytic Kolmogorov inertial-range model, to that calculated from our standard density-entropy (Eq. 14) and pressure-entropy (Eq. 21) formulations. The mean softening length *h* is shown as the vertical dotted line. Both do well down to a few softenings, where they first fall below the analytic result (excess dissipation) then rise above (kernel-scale noise). The EOM choice has a weak effect on the results. We compare different SPH algorithms and codes (description in text); agreement is good where the same methods are used. The "PHANTOM" and "GADGET-3 with Memior? AN" we a dwarf of the simulation of the simulation of the simulation.

# Summary: Advantages and disadvantages of SPH

#### Advantages:

3.0

- Resolution follows mass
- Zero dissipation until explicitly added
- Exact and simultaneous conservation of all physical quantities is possible
- Intrinsic remeshing procedure
- Does not crash

#### Disadvantages:

- Resolution follows mass
- Dissipation terms must be explicitly added to treat discontinuities
   methods can be crude (need a good switch)
- Exact conservation no guarantee of accuracy
- Screw-ups indicated by noise rather than code crash

Historical difficulties incorporating magnetic fields (MHD)

# Magnetic fields in SPH: recent progress

![](_page_29_Picture_1.jpeg)

Price, Tricco & Bate (2012, MNRAS Lett.); Tricco & Price (2012, J. Comp. Phys.)

# What is the future for SPH in numerical cosmology?

#### Recent key advances:

- Cullen & Dehnen (2010), Read & Heyfield (2011): state-of-the-art viscosity switches now capable of completely removing spurious effects of artificial viscosity away from shocks
- Dehnen & Aly (2012): pairing instability can be solved using Wendland kernels
- Tricco & Price (2012): New divergence cleaning scheme for SPMHD, we can do MHD in SPH for the first time with no limitations

## Myths and misconceptions:

- Will carry on, it's the method everybody loves to hate
- SPH is deceptively simple to implement, much more difficult to master
- "Fundamental problems" have so far turned out to be rather elementary issues common to all numerical methods